

# CE 415 DESIGN OF STEEL STRUCTURES LECTURE 3 TENSION MEMBER

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#### **LRFD** Design

 $\phi_t T_n \ge T_u$  Where,

 $\phi_t$  = resistance factor relating to tension member strength

 $T_n$  = nominal strength of a tension member (see AISC-Chapter D)

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 $\phi_t T_n$  = design strength of a tension member

 $T_u$  = factored load on a tension member

#### **Tension Members have THREE limit states:**

- 1. Yielding on gross section
- 2. Fracture on effective section
- 3. Block Shear

**Yielding on gross section** 

 $\phi_t T_n = \phi_t F_y A_g = 0.9 \, F_y A_g$ 

Fracture on effective net section

 $\phi_t T_n = \phi_t F_u A_e = 0.75 F_u A_e$ 

Note that the resistance factor  $\phi_t$  is 0.90 for the yielding limit state and 0.75 for the fracture limit state.

#### ASD Design

**Yielding on gross section** 

Nominal Strength:  $T_n = F_y A_g$ 

Allowable Strength:  $\frac{T_n}{\Omega} = \frac{F_y A_g}{\Omega} = \frac{F_y A_g}{1.67}$ 

Safety factor  $\Omega$  = 1.67 for yielding on gross section

Fracture on effective net section

Nominal Strength:  $T_n = F_u A_e$ 

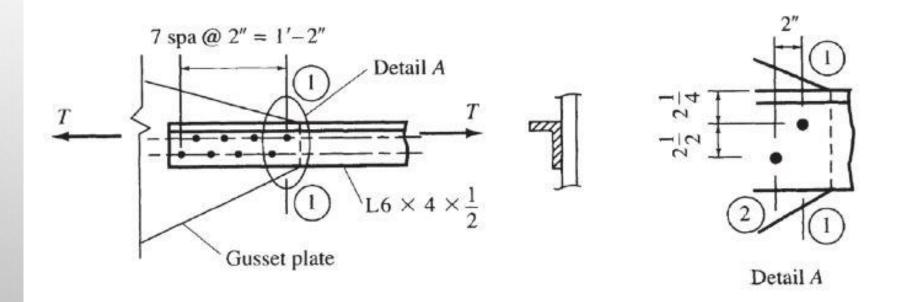
Allowable Strength:  $\frac{T_n}{\Omega} = \frac{F_u A_e}{\Omega} = \frac{F_u A_e}{2.00}$ 

Safety factor  $\Omega$  = 2.00 for fracture on net section

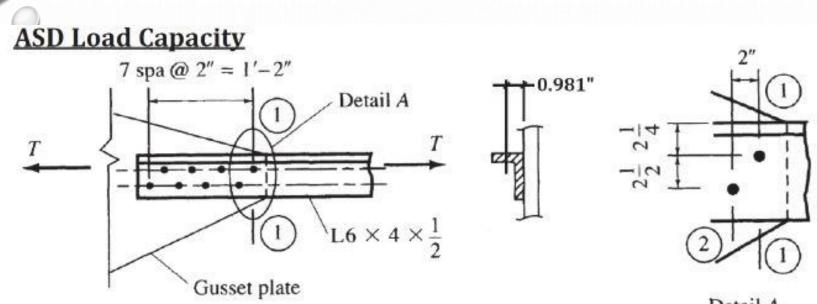
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#### ASD Load Capacity

Determine the service load capacity in tension for an L6 x 4 x  $^{1}/_{2}$  A572 Grade 50 steel connected with  $^{7}/_{8}$  -in.-diam. bolts in standard holes as shown. Assume live load to be three times the dead load. Neglect block shear failure.



| Designation  |       |   |         |   |   | A          | 1x        | rx    | у     | ly    | ry    | x     |
|--------------|-------|---|---------|---|---|------------|-----------|-------|-------|-------|-------|-------|
| L 9x4x1      | 9     | х | 4       | х | 1                                       | 12.0       | 97.0      | 2.84  | 3.50  | 12.0  | 1.00  | 1.00  |
| L 7x4x0.625  | 7     | х | 4 :     | х | 5/8                                     | 6.48       | 32.4      | 2.24  | 2.46  | 7.84  | 1.10  | 0.963 |
| L 6x4x0.75   | 6     | х | 4 :     | х | 3/4                                     | 6.94       | 24.5      | 1.88  | 2.08  | 8.68  | 1.12  | 1.08  |
| L 6x4x0.625  | 6     | х | 4 :     | х | 5/8                                     | 5.86       | 21.1      | 1.90  | 2.03  | 7.52  | 1.13  | 1.03  |
| L 6x4x0.5625 | 6     | x | 4       | х | 9/16                                    | 5.31       | 19.3      | 1.90  | 2.01  | 6.91  | 1.14  | 1.01  |
| L 6x4x0.5    | 6     | x | 4       | x | 1/2                                     | 4.75       | 17.4      | 1.91  | 1.99  | 6.27  | 1.15  | 0.987 |
| 6x4x0.4375   | 6     | х | 4 :     | х | 7/16                                    | 4.18       | 15.5      | 1.92  | 1.96  | 5.60  | 1.16  | 0.964 |
| 6x4x0.375    | 6     | х | 4 :     | х | 3/8                                     | 3.61       | 13.5      | 1.93  | 1.94  | 4.90  | 1.17  | 0.941 |
| 4x3.5x0.437  | 4     | х | 3 1/2   | х | 7/16                                    | 3.09       | 4.76      | 1.24  | 1.23  | 3.40  | 1.05  | 0.978 |
| 4x3.5x0.375  | 4     | х | 3 1/2 : | х | 3/8                                     | 2.67       | 4.18      | 1.25  | 1.21  | 2.95  | 1.06  | 0.955 |
| 4x3.5x0.312  | 4     | х | 3 1/2 : | х | 5/16                                    | 2.25       | 3.56      | 1.26  | 1.18  | 2.55  | 1.07  | 0.932 |
| 4x3.5x0.25   | 4     | х | 3 1/2 : | х | 1/4                                     | 1.81       | 2.91      | 1.27  | 1.16  | 2.09  | 1.07  | 0.909 |
| 4x3x0.625    | 4     | х | 3 :     | х | 5/8                                     | 3.98       | 6.03      | 1.23  | 1.37  | 2.87  | 0.849 | 0.871 |
| L 4x3x0.5    | 4     | x | 3 :     | х | 1/2                                     | 3.25       | 5.05      | 1.25  | 1.33  | 2.42  | 0.864 | 0.827 |
| 4x3x0.4375   | 4     | х | 3 :     | х | 7/16                                    | 2.87       | 4.52      | 1.25  | 1.30  | 2.18  | 0.871 | 0.804 |
| 4x3x0.375    | 4     | х | 3 :     | x | 3/8                                     | 2.48       | 3.96      | 1.26  | 1.28  | 1.92  | 0.879 | 0.782 |
| 3.5x2.5x0.2  | 3 1/2 | х | 2 1/2   | х | 1/4                                     | 1.44       | 1.8       | 1.12  | 1.11  | 0.777 | 0.735 | 0.614 |
| 3x2.5x0.5    | 3     | х | 2 1/2   | х | 1/2                                     | 2.50       | 2.08      | 0.913 | 1.00  | 1.30  | 0.722 | 0.750 |
| 3x2.5x0.437  | 3     | х | 2 1/2 : | х | 7/16                                    | 2.21       | 1.88      | 0.920 | 0.978 | 1.18  | 0.729 | 0.728 |
| 3x2.5x0.375  | 3     | х | 2 1/2 : | х | 3/8                                     | 1.92       | 1.66      | 0.928 | 0.956 | 1.04  | 0.736 | 0.706 |
| 3x2.5x0.312  | 3     | х | 2 1/2 : | х | 5/16                                    | 1.62       | 1.42      | 0.937 | 0.933 | 0.898 | 0.744 | 0.683 |
| 3x2.5x0.25   | 3     | x | 2 1/2   | x | 1/4                                     | 1.31       | 1.17      | 0.945 | 0.911 | 0.743 | 0.753 | 0.661 |
|              |       |   |         | - | 100000000000000000000000000000000000000 | 100 202-00 | 200 C 200 |       |       |       |       |       |



Detail A

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Consider net section along 1-1 and along 1-2, because at these two sections, full force is transferred.

From AISC Manual:  $A_q = 4.75$  in<sup>2</sup> and  $\overline{x} = 0.981$ 

Along 1-1: 
$$A_n = A_g - (1-\text{hole}) = 4.75 - (7/8 + 1/8) \times (1/2) = 4.25 \text{ in}^2$$
  
Along 1-2:  $A_n = A_g - (2-\text{hole}) + s^2/4g$   
 $= 4.75 - 2(7/8 + 1/8) \times (1/2) + 2^2/(4 \times 2.5)(1/2)$   
 $= 3.95 \text{ in}^2$   
 $U = 1 - \overline{x}/L = 1 - 0.981/14 = 0.93$   
 $A_e = UA_n = 0.93 \times 3.95 = 3.67 \text{ in}^2$ .

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## ASD Load Capacity

A572 Grade 50 steel:  $F_v = 50$  ksi,  $F_u = 65$  ksi.

<u>Yielding on gross area:</u> Allowable tension =  $T_n/\Omega = F_y A_g/\Omega = 50(4.75)/1.67 = 142$  kips

<u>Fracture on effective area:</u> Allowable tension =  $T_n/\Omega = F_u A_e/\Omega = 65(3.67)/2.00 = 119$  kips  $\rightarrow$  Governs

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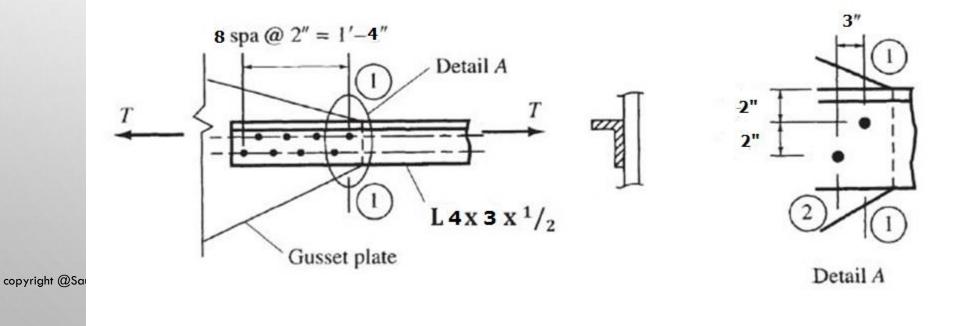
Now, D + L = 119  $\Rightarrow D + 3D = 119$  $\Rightarrow D = 29.75$  kips

 $\therefore L = 3D = 89.25$  kips

# SUBMIT THE ASSIGNMENT IN MOODLE

### ASD Load Capacity

Determine the service load capacity in tension for an L 4x 3 x  $^{1}/_{2}$  A572 Grade 50 steel connected with  $^{5}/_{8}$  -in.-diam. bolts in standard holes as shown. Assume live load to be two times the dead load. Neglect block shear failure.



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## □ SUBMIT THE ASSIGNMENT IN MOODLE

**USE ANGLE PROPERTY TABLE** 

**SOLVE THE MATH** 

WRITE STUDENT ID

TAKE PICTURE OF THE ASSIGNMENT

UPLOAD IT IN THE MOODLE SITE.