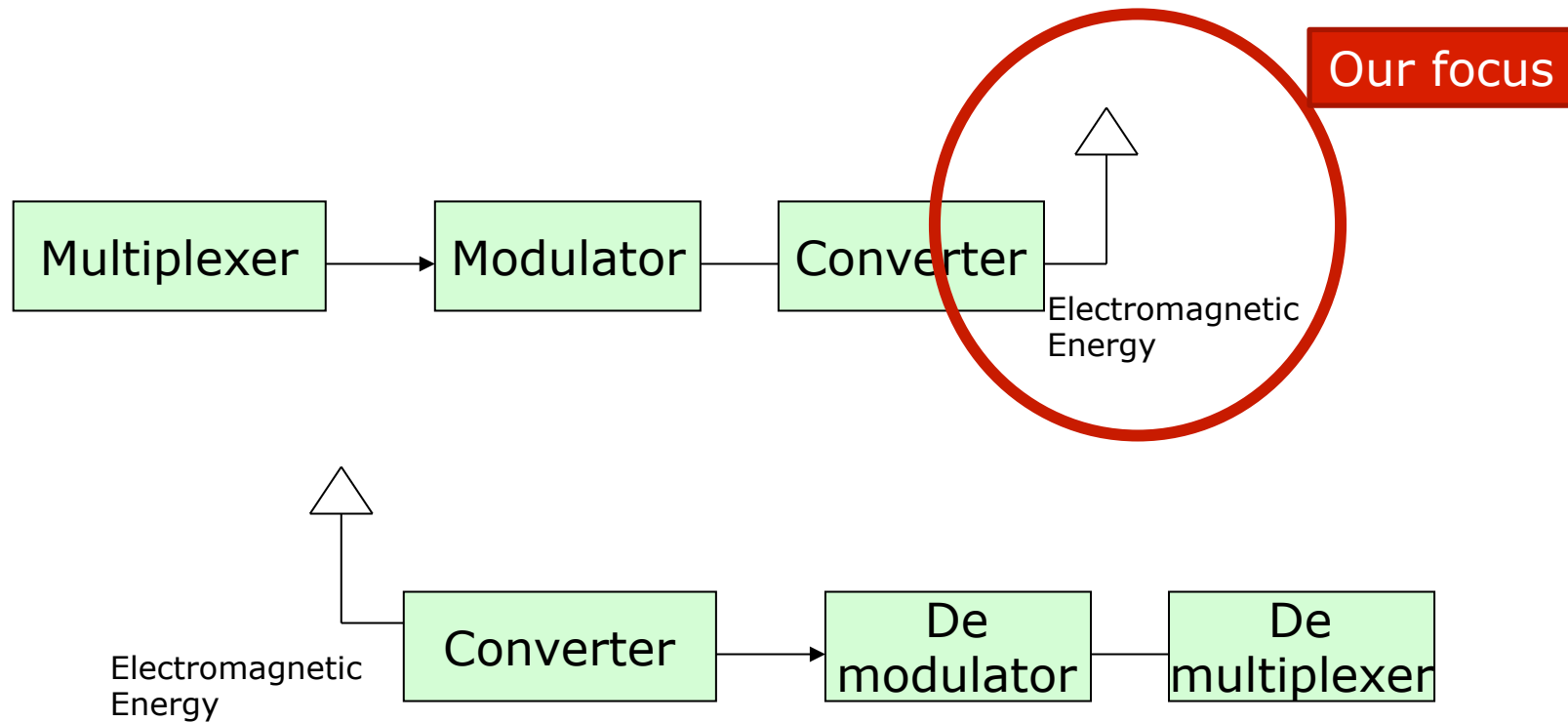


Antennas and Propagation

updated: 09/29/2014

Wireless Communication Systems

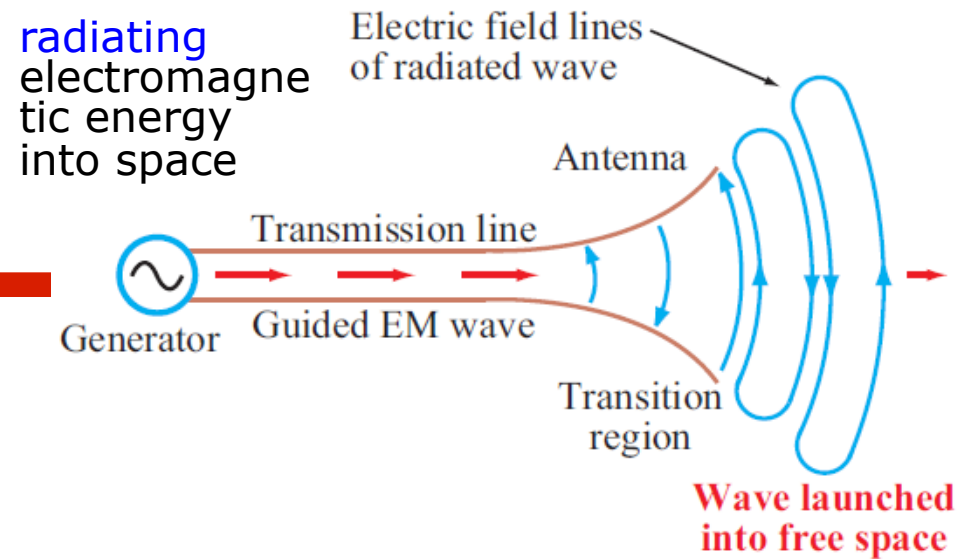


Antenna Characteristics

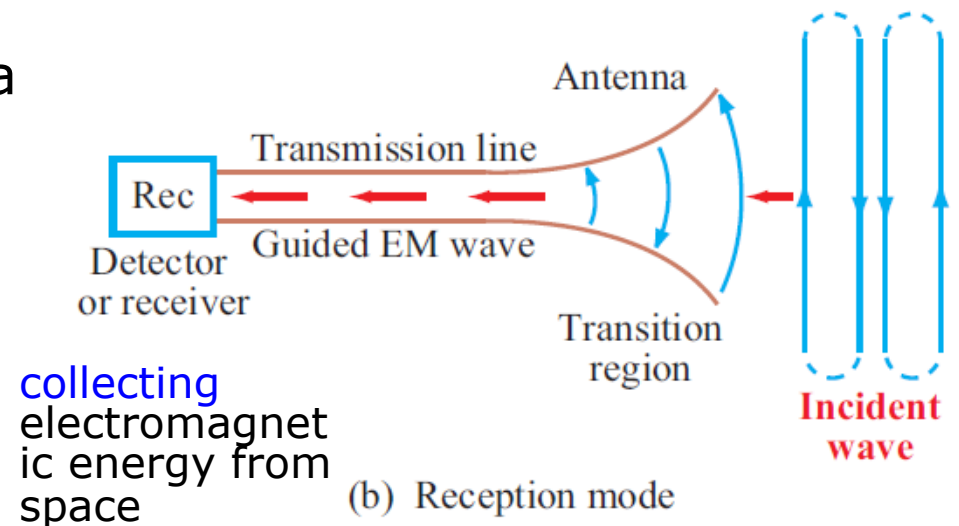
- ❑ Radiation patterns
 - ❑ Radiated power
 - ❑ Half-power beam width of the antenna
 - ❑ Antenna position, shape, and length
 - ❑ Antenna gain with respect to an ideal case
-

Remember: Antenna Properties

- An antenna is an electrical conductor (transducer) or system of conductors
 - They carry **time-varying currents** and, consequently, accelerating electrons
 - → A Transmission Antenna **radiates** electromagnetic energy into space
 - → A Reception Antenna collects electromagnetic energy from space

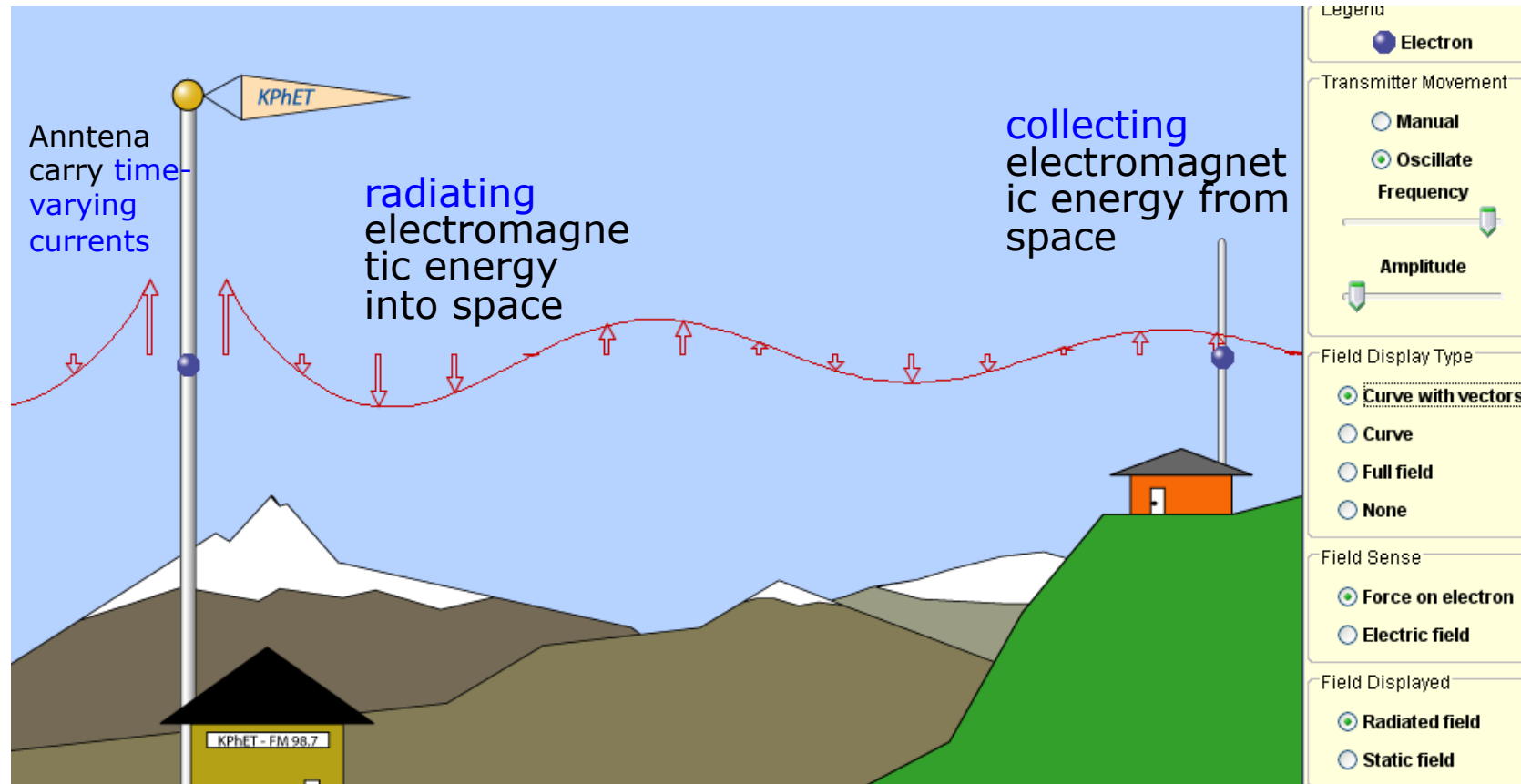


(a) Transmission mode



(b) Reception mode

Remember: Waves and Propagation - Demo



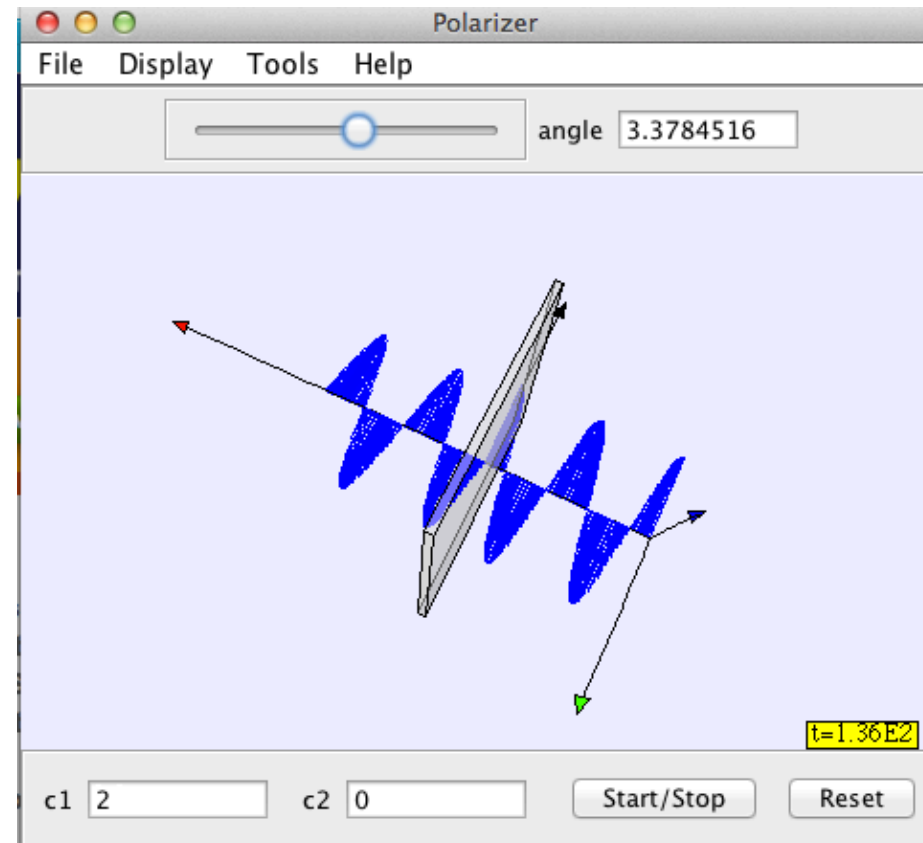
[http://phet.colorado.edu/simulations/sims.php?sim=Radio Waves and Electromagnetic Fields](http://phet.colorado.edu/simulations/sims.php?sim=Radio+Waves+and+Electromagnetic+Fields)

Remember: Antenna Properties

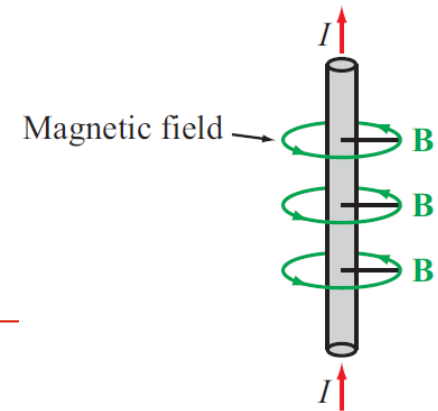
Reciprocal Devices

- Most antennas are **reciprocal devices**,
 - That is they are exhibiting the **same radiation pattern** for transmission as for reception
 - When operating in the receiving mode, the antenna captures the incident wave
 - Only that component of the wave whose electric field matches the antenna **polarization state** is detected
 - In two-way communication, the same antenna can be used for transmission and reception
 - Antenna characteristics are the same for transmitting or receiving electromagnetic energy
 - The antenna can receive on one **frequency** and transmit on another
-

Polarization



Start With Basics:

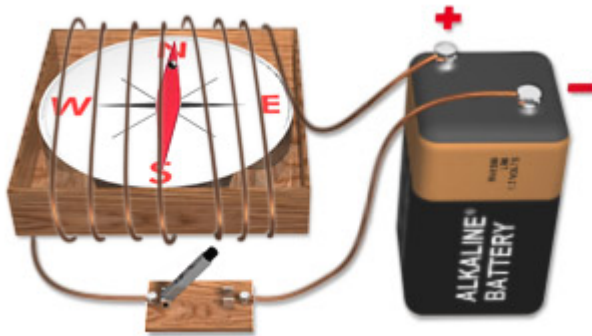


- We know:
 - Q (static charges) \rightarrow E field– capacitor example[1]
 - I (moving charges) \rightarrow H field– compass example[2]
 - Thus, in the presence of time-varying current \rightarrow we will obtain interdependent EM fields
- A time-varying current (**I**) along a wire generates **rings of Electromagnetic field (B)** around the wire
- Similarly the current passing through a coil generates Electromagnetic field in the Z axis

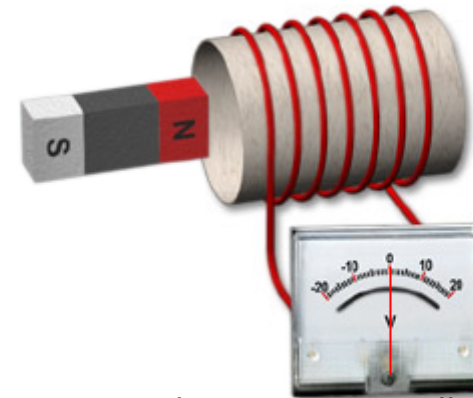
[2] <http://micro.magnet.fsu.edu/electromag/java/compass/index.html>

[1] <http://micro.magnet.fsu.edu/electromag/electricity/capacitance.html>

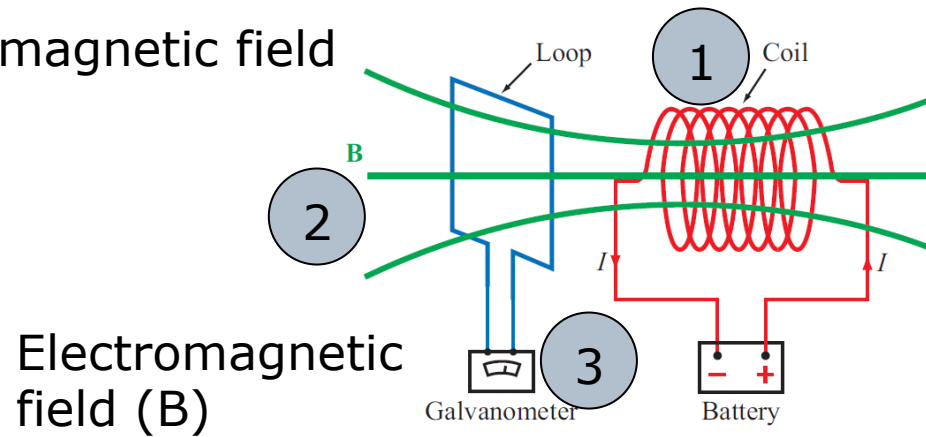
Simple Experiments



An induced magnetic field



Galvanometer needle moves



Electromagnetic field (B)

Faraday confirmed that a moving magnetic field is necessary in order for electromagnetic induction to occur

Faraday's Law: Electromotive force (voltage) induced by time-varying magnetic flux:

Maxwell Equations

- Gauss's Law
- Faraday's Law
- Gauss's Law for Magnetism
- Ampere's Law

Relationships between charges, current, electrostatic, electromagnetic, electromotive force!

POINT FORM	INTEGRAL FORM
$\nabla \times \mathbf{H} = \mathbf{J}_c + \frac{\partial \mathbf{D}}{\partial t}$	$\oint \mathbf{H} \cdot d\mathbf{l} = \int_S \left(\mathbf{J}_c + \frac{\partial \mathbf{D}}{\partial t} \right) \cdot d\mathbf{S}$ (Ampère's law)
$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$	$\oint \mathbf{E} \cdot d\mathbf{l} = \int_S \left(-\frac{\partial \mathbf{B}}{\partial t} \right) \cdot d\mathbf{S}$ (Faraday's law; S fixed)
$\nabla \cdot \mathbf{D} = \rho$	$\oint_S \mathbf{D} \cdot d\mathbf{S} = \int_V \rho \, dv$ (Gauss's law)
$\nabla \cdot \mathbf{B} = 0$	$\oint_S \mathbf{B} \cdot d\mathbf{S} = 0$ (nonexistence of monopole)

Maxwell's Equations – Free Space Set

- We assume there are **no charges** in free space
and $J_c = \sigma E = 0$

POINT FORM	INTEGRAL FORM
$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t}$	$\oint \mathbf{H} \cdot d\mathbf{l} = \int_s \left(\frac{\partial \mathbf{D}}{\partial t} \right) \cdot d\mathbf{S}$
$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$	$\oint \mathbf{E} \cdot d\mathbf{l} = \int_s \left(-\frac{\partial \mathbf{B}}{\partial t} \right) \cdot d\mathbf{S}$
$\nabla \cdot \mathbf{D} = 0$	$\oint_s \mathbf{D} \cdot d\mathbf{S} = 0$
$\nabla \cdot \mathbf{B} = 0$	$\oint_s \mathbf{B} \cdot d\mathbf{S} = 0$

Time-varying E and H cannot exist independently!

If dE/dt non-zero \rightarrow
 dD/dt is non-zero
 \rightarrow Curl of H is non-zero
 \rightarrow D is non-zero
 (Amp. Law)

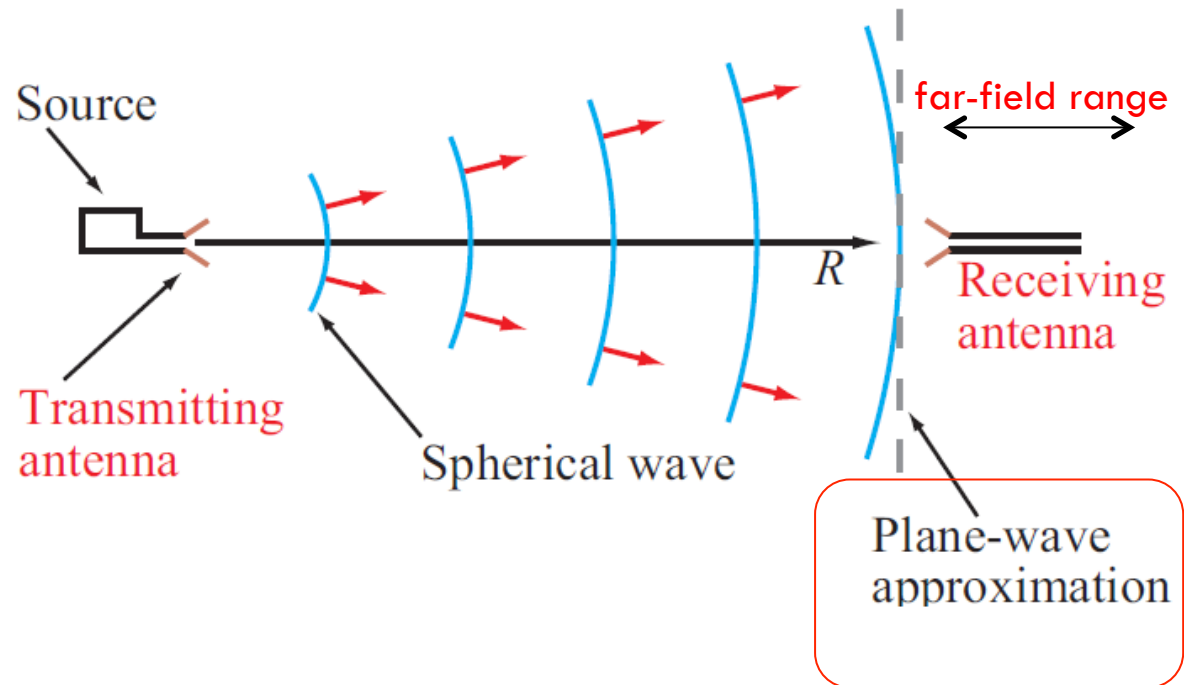
If H is a function of time \rightarrow E must exist!
 (Faraday's Law)

Interrelating magnetic and electric fields!

Our Focus: Far-Field Approximation

$$d_{\text{far_field}} = (2 \cdot l^2) / \lambda$$

1. In close proximity to a radiating source, the wave is **spherical** in shape, but at a far distance, it becomes approximately a **plane wave** as seen by a receiving antenna.
2. The far-field approximation **simplifies the math**.
3. The distance beyond which the far-field approximation is valid is called the **far-field range** (will be defined later).

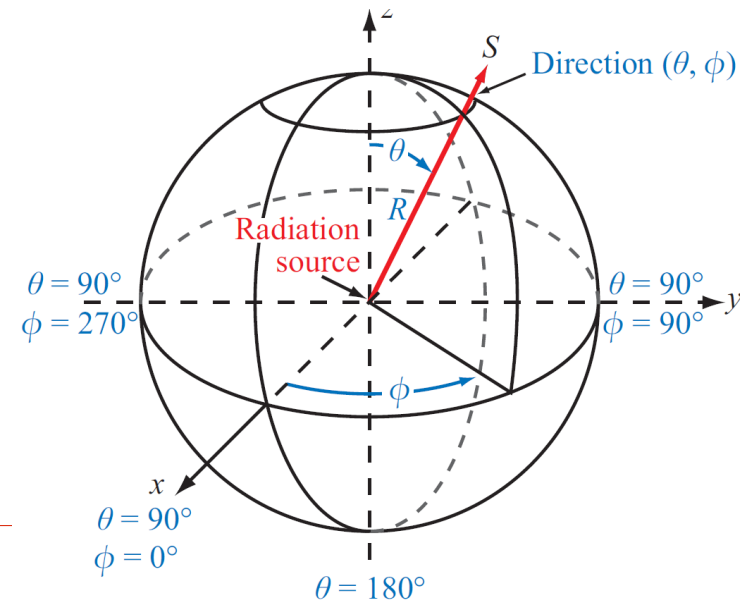
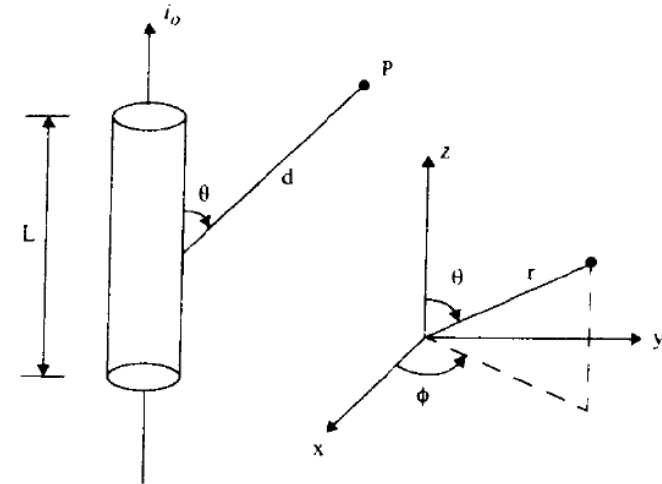


Very similar to throwing a stone in water!

What is the power radiated?

A far field approximation

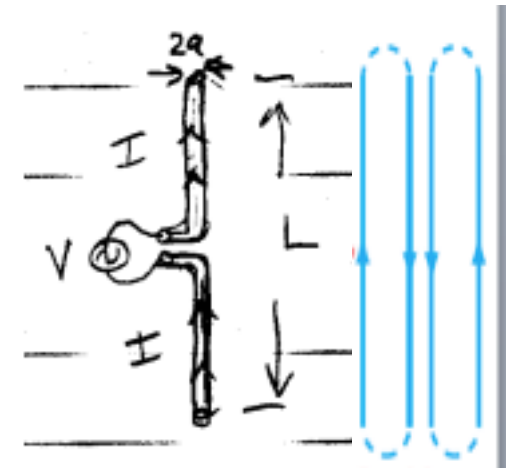
- Assuming the alternating current travels in Z direction \rightarrow radiated power must be in Z
- Antenna patterns are represented in a **spherical coordinate** system
- Thus, variables $R, \theta, \phi \rightarrow$
 - range,
 - zenith angle (elevation),
 - azimuth angle



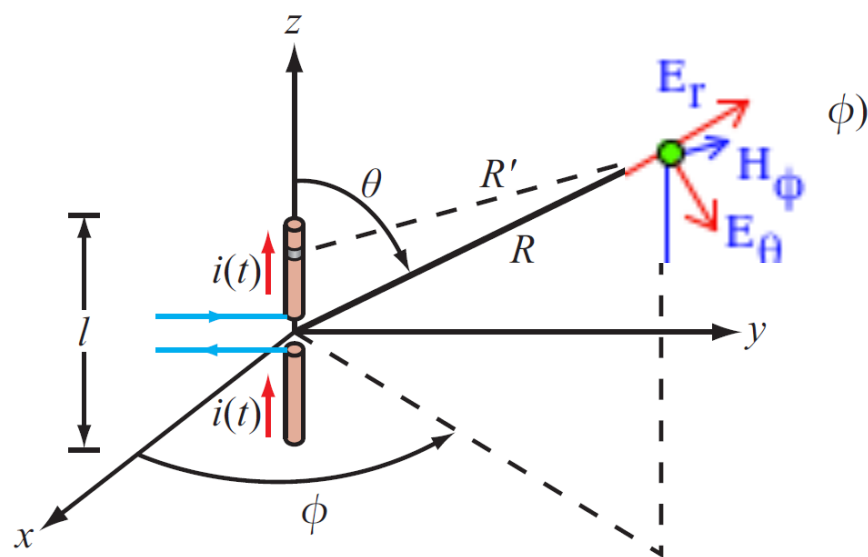
Hertzian Dipole Antenna

- Using Ampere's Law
- But how is the current $I(r)$ distributed on the antenna?
- One way to approximate this rather difficult problem is to use thin-wire dipole antenna approximation
 - Dipole because we have two poles (wires)
 - $a \ll L$
- We only consider the case when L is very very short (Hertzian Dipole)
 - Infinitesimally short
 - Uniform current distribution

$$\vec{E}(\vec{r}) = \frac{1}{j\omega\epsilon} \nabla \times \vec{H}(\vec{r})$$



Hertzian Dipole (Differential Antenna) Radiation Properties

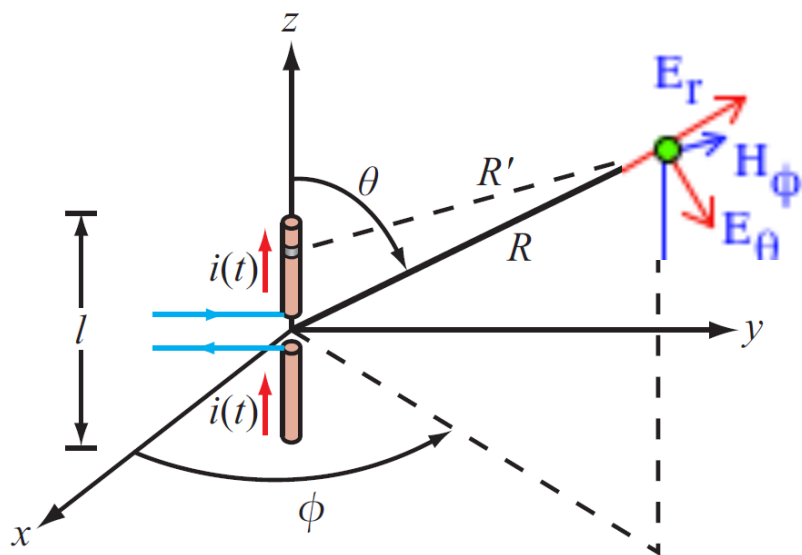


$$i(t) = I_0 \cos \omega t = \Re[I_0 e^{j\omega t}]$$

- Very thin, short ($l < \lambda/50$) linear conductor
- Observation point is somewhere in the space

<http://www.amanogawa.com/archive/Antenna1/Antenna1-2.html>

Hertzian Dipole (Differential Antenna) Radiation Properties



$$\tilde{H}_\phi = \frac{I_0 l k^2}{4\pi} e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} \right] \sin \theta,$$

$$\tilde{E}_R = \frac{2I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \cos \theta,$$

$$\tilde{E}_\theta = \frac{I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \sin \theta$$

Note that:

$$\omega = 2\pi f;$$

$$k = \omega / c = 2\pi f / c = 2\pi / \lambda;$$

$$l \ll \lambda / 50; \quad K = \text{wave number}$$

$$R \approx R' = \Gamma;$$

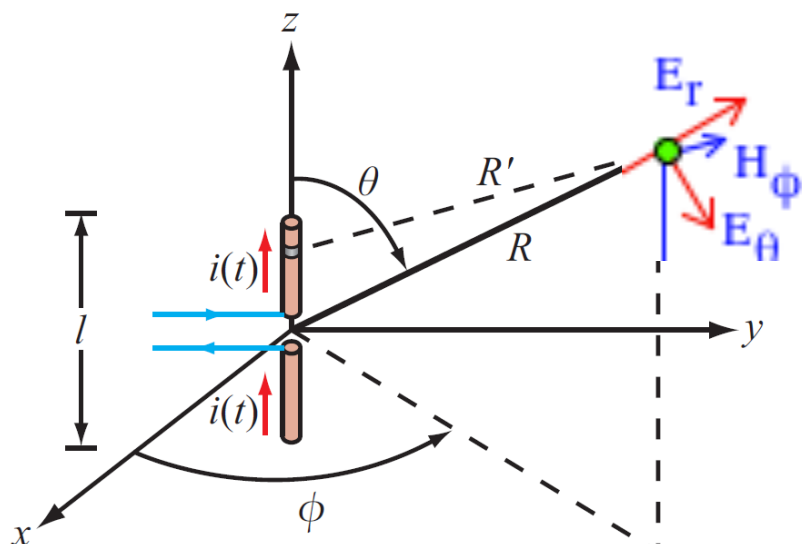
$$\eta_0 = \sqrt{\mu_0 / \epsilon_0} = 120\pi;$$

ϵ is the free space permittivity (about 1)

μ is magnetic Permeability

η is the intrinsic impedance in Ohm

Hertzian Dipole (Differential Antenna) Radiation Properties



$$\tilde{H}_\phi = \frac{I_0 l k^2}{4\pi} e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} \right] \sin\theta, \text{ A/m}$$

$$\tilde{E}_R = \frac{2I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \cos\theta,$$

$$\tilde{E}_\theta = \frac{I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \sin\theta \text{ V/m}$$

In this case:

$1/R \rightarrow$ radiation field components

$1/R^2 \rightarrow$ induction field components

$1/R^3 \rightarrow$ electrostatic field components

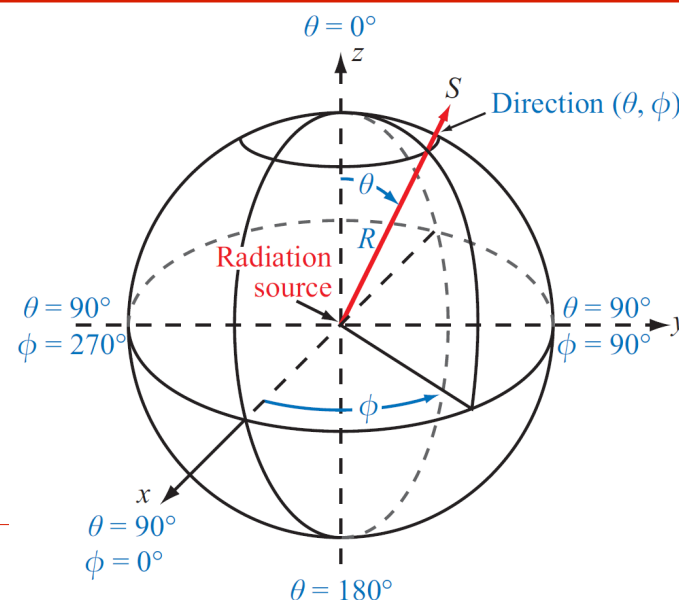
Far-field \rightarrow only radiation field!

\rightarrow **Only E_θ and H_ϕ will be significant!**

$R =$ Range

$\theta =$ Zenith (elevation) – side view

$\phi =$ Azimuth – top view



Hertzian Dipole (Differential Antenna) Radiation Properties

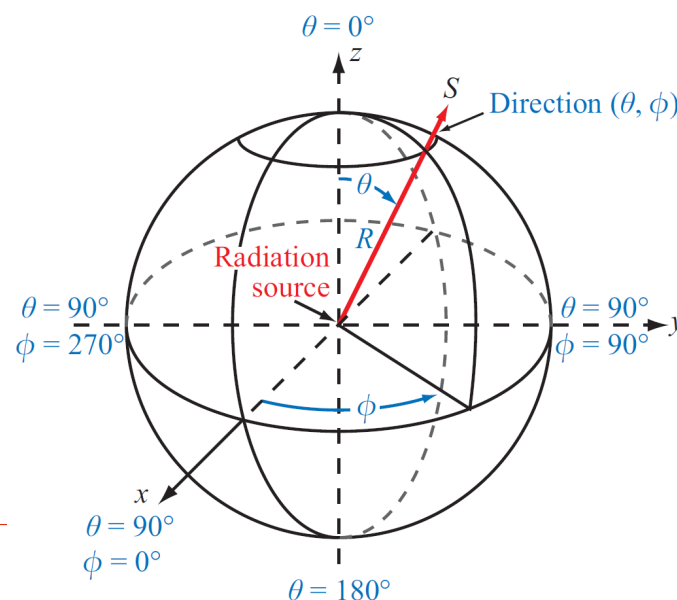
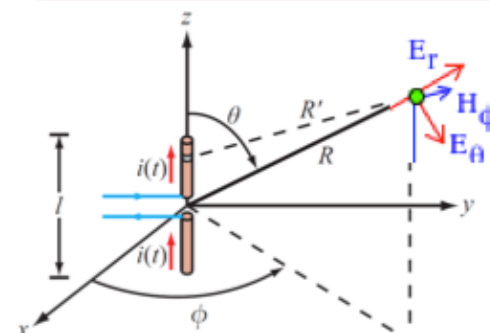
$$\tilde{H}_\phi = \frac{I_0 l k^2}{4\pi} e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} \right] \sin \theta, \text{ A/m}$$

$$\tilde{E}_R = \frac{2I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \cos \theta,$$

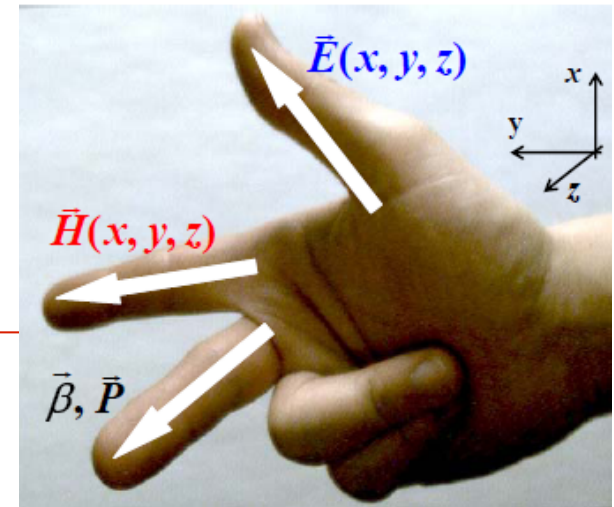
$$\tilde{E}_\theta = \frac{I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \sin \theta \text{ V/m}$$

$$\tilde{E}_\theta = \frac{jI_0 l k \eta_0}{4\pi} \left(\frac{e^{-jkR}}{R} \right) \sin \theta \quad (\text{V/m}),$$

$$\tilde{H}_\phi = \frac{\tilde{E}_\theta}{\eta_0} \quad (\text{A/m}),$$



Radiated Power Flux Density



Electric and Magnetic Intensity Fields ($E_R \sim 0$)

$$\tilde{E}_\theta = \frac{jI_0 l k \eta_0}{4\pi} \left(\frac{e^{-jkR}}{R} \right) \sin \theta \quad (\text{V/m}),$$

$$\tilde{H}_\phi = \frac{\tilde{E}_\theta}{\eta_0} \quad (\text{A/m}),$$

Average Power flux Density

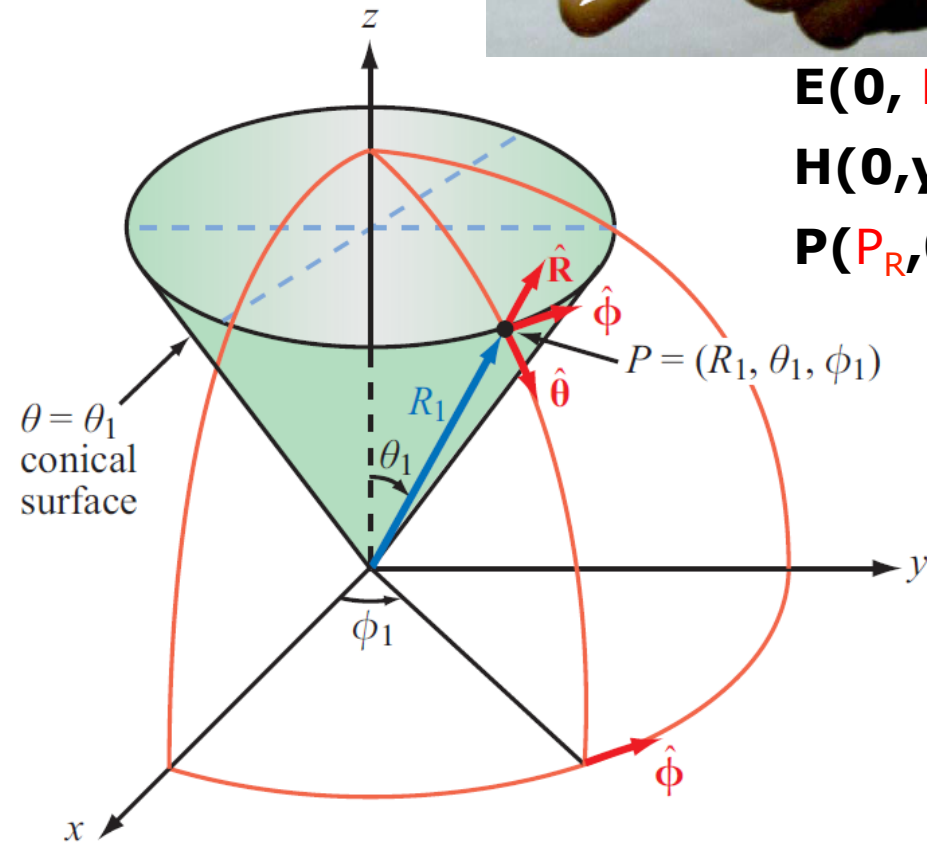
$$\mathbf{S}_{\text{av}} = \frac{1}{2} \Re \left(\tilde{\mathbf{E}} \times \tilde{\mathbf{H}}^* \right) \quad (\text{W/m}^2).$$

$$\mathbf{S}_{\text{av}} = \hat{\mathbf{R}} S(R, \theta),$$

Cross product of E and H

$$S(R, \theta) = \left(\frac{\eta_0 k^2 I_0^2 l^2}{32\pi^2 R^2} \right) \sin^2 \theta$$

$$= S_0 \sin^2 \theta \quad (\text{W/m}^2).$$



$$\mathbf{E}(\mathbf{0}, E_\theta, \mathbf{0})$$

$$\mathbf{H}(\mathbf{0}, y, H_\phi)$$

$$\mathbf{P}(P_R, \mathbf{0}, z)$$

Normalized Radiation Intensity(F)

Normalized Radiation Intensity

→ How much radiation in each direction?

$$F(\theta, \phi) = \frac{S(R, \theta, \phi)}{S_{\max}} \quad (\text{dimensionless})$$

$$F(\theta, \phi) = F(\theta) = \sin^2 \theta$$

$$S(R, \theta) = \left(\frac{\eta_0 k^2 I_0^2 l^2}{32\pi^2 R^2} \right) \sin^2 \theta$$

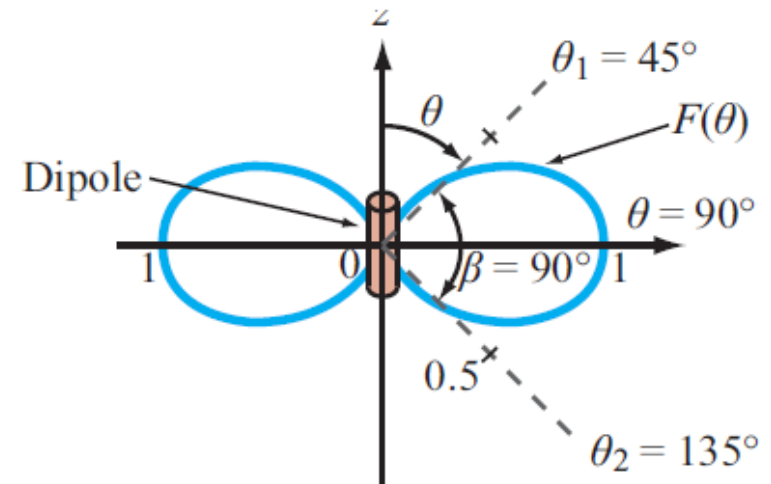
$$= S_0 \sin^2 \theta \quad (\text{W/m}^2).$$

$S_0 = S_{\max} = \text{Max. Power Density}$

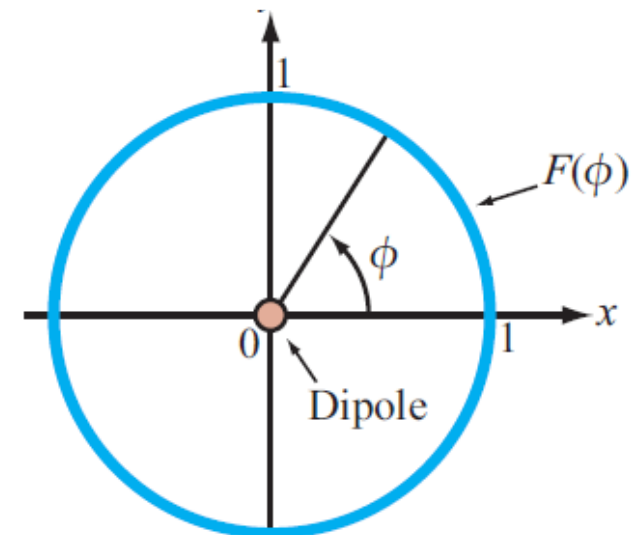
R= Range

θ =Zenith (elevation) – side view

ϕ =Azimuth – top view



Elevation Pattern
(side view)



Azimuth Pattern
(top view)

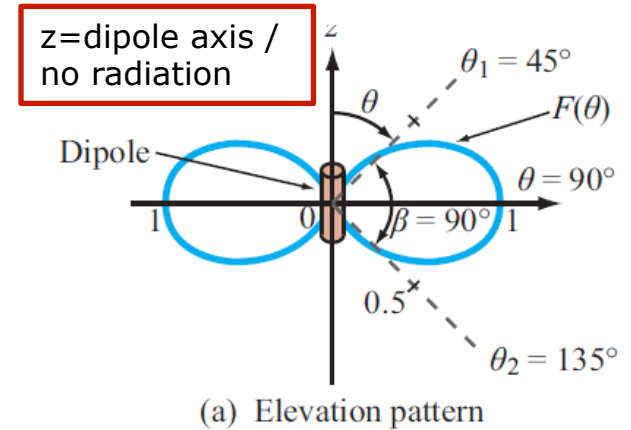
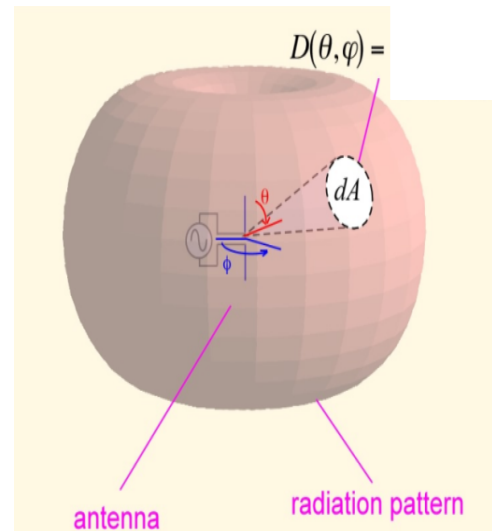
Radiation Pattern of Hertzian (short) Dipole

$$F(\theta, \phi) = \frac{S(R, \theta, \phi)}{S_{\max}}$$

$$F(\theta, \phi) = F(\theta) = \sin^2 \theta$$

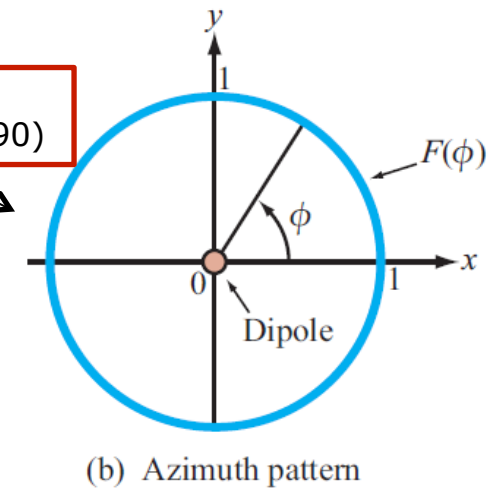
Note:

$F(\theta, \phi) = 1$ for isotropic antenna

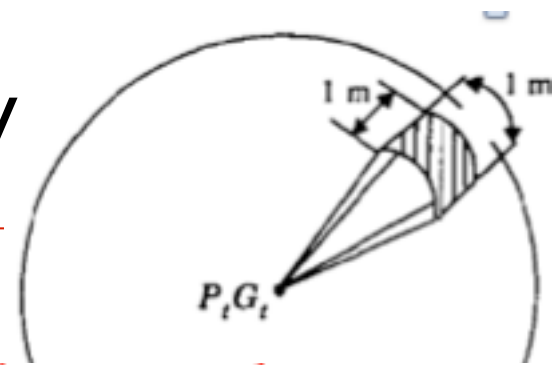


Maximum radiation
In the broadside direction ($\theta = 90^\circ$)

Doughnut-shaped radiation
pattern in θ - ϕ space



Connecting The Dots: Radiated Power Flux Density



Electric and Magnetic Intensity Fields ($E_r \sim 0$)

$$\tilde{E}_\theta = \frac{jI_0 l k \eta_0}{4\pi} \left(\frac{e^{-jkR}}{R} \right) \sin \theta \quad (\text{V/m}),$$

$$\tilde{H}_\phi = \frac{\tilde{E}_\theta}{\eta_0} \quad (\text{A/m}),$$

Antenna	Power Gain	Effective Area
Isotropic	1	$\lambda^2/(4\pi)$

Average Power flux Density

$$\mathbf{S}_{av} = \frac{1}{2} \Re \left(\tilde{\mathbf{E}} \times \tilde{\mathbf{H}}^* \right) \quad (\text{W/m}^2).$$

$$\mathbf{S}_{av} = \hat{\mathbf{R}} S(R, \theta),$$

Cross product of E and H

$$S(R, \theta) = \left(\frac{\eta_0 k^2 I_0^2 l^2}{32\pi^2 R^2} \right) \sin^2 \theta$$

$$= S_0 \sin^2 \theta \quad (\text{W/m}^2).$$

For Isotropic Antenna We Obtain:

$$S_{av} = P_{den} = \frac{E^2}{\eta_0} = \frac{E^2}{120\pi} = \frac{EIRP}{4\pi \cdot d^2} \quad \text{W/m}^2$$

$$P_r = P_{den} \cdot A_{er} = \frac{P_t \cdot G_t \cdot G_r \cdot \lambda^2}{(4\pi)^2 \cdot d^2} = \frac{E^2}{120\pi} \times A_{er} \quad \text{W}$$

Note:

S_{av} is the average power radiated or pwr density radiated by an isotropic antenna

EIRP is the total power radiated

P_{den} is power flux density

Example

- Example A (Hertzian Dipole)
 - Example B (Isotropic Antenna)
-

Antenna Directionality

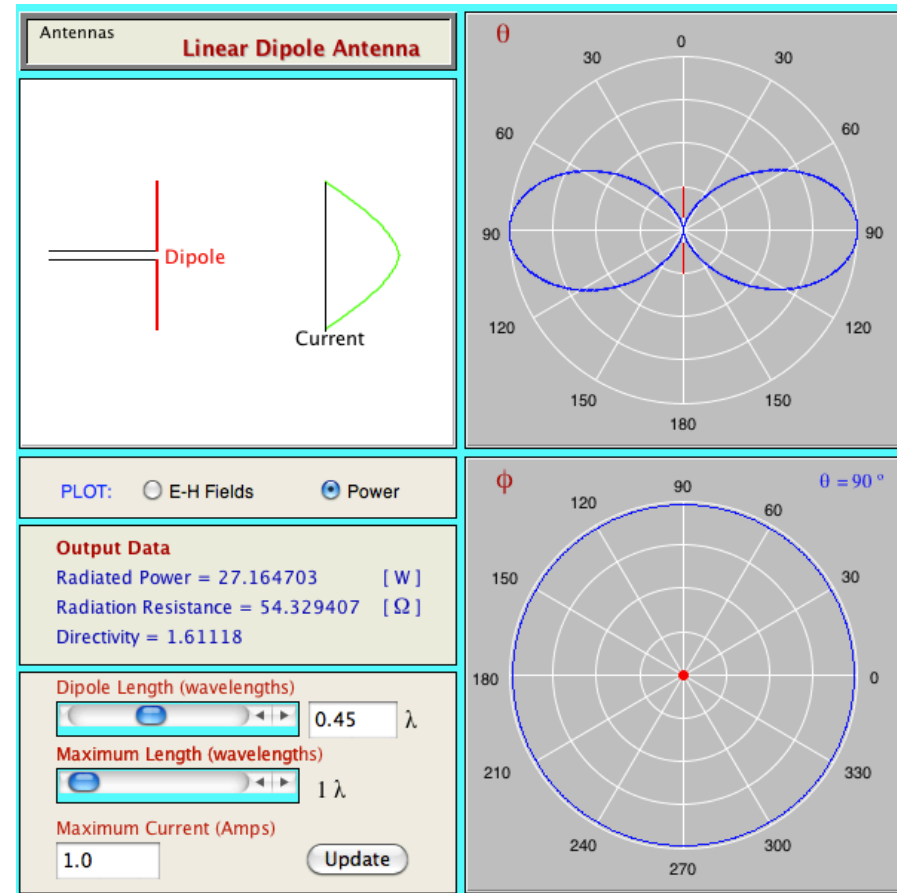
- Set the wavelength to 1
- Set Current to 1 A
- Plot Power
- Change the length
- Q1: What happens to the directivity when I changes?
- Q2: What happens to the power when L changes?

The magic is all here:

$$\tilde{H}_\phi = \frac{I_0 l k^2}{4\pi} e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} \right] \sin \theta,$$

$$\tilde{E}_R = \frac{2I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \cos \theta,$$

$$\tilde{E}_\theta = \frac{I_0 l k^2}{4\pi} \eta_0 e^{-jkR} \left[\frac{j}{kR} + \frac{1}{(kR)^2} - \frac{j}{(kR)^3} \right] \sin \theta$$

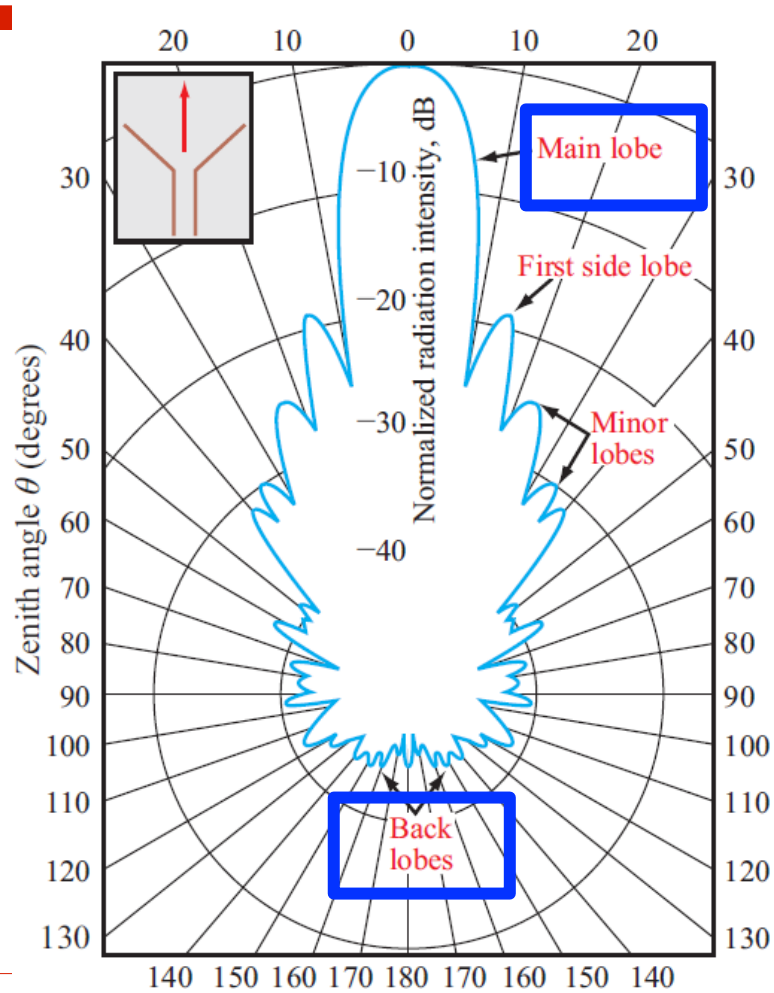


Other Antenna Properties

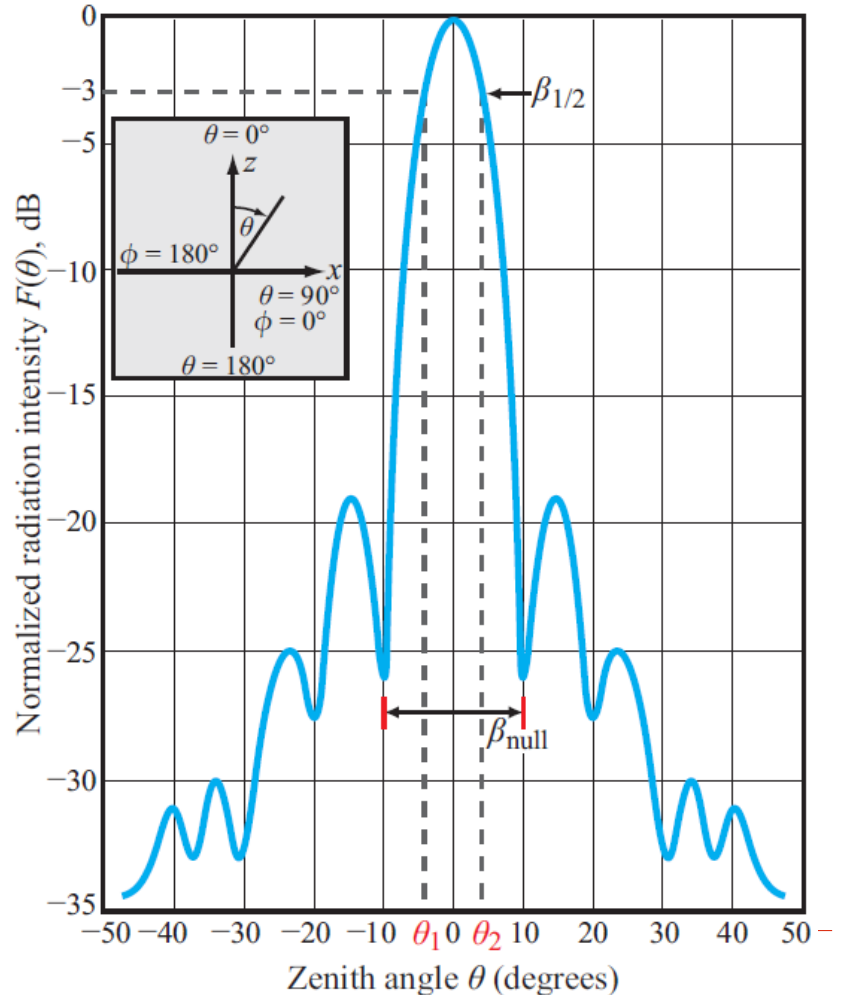
- We already looked at the radiation intensity and radiation pattern
 - Other properties
 - Radiation Pattern Characteristics
 - Radiation Resistance
-

Radiation Pattern – Polar and Rectangular Plots

- Principal planes:**
- Elevation plane** (x-z and y-z planes) - sides
 - Azimuth plane** (x-y plane) - top



(a) Polar diagram



(b) Rectangular plot

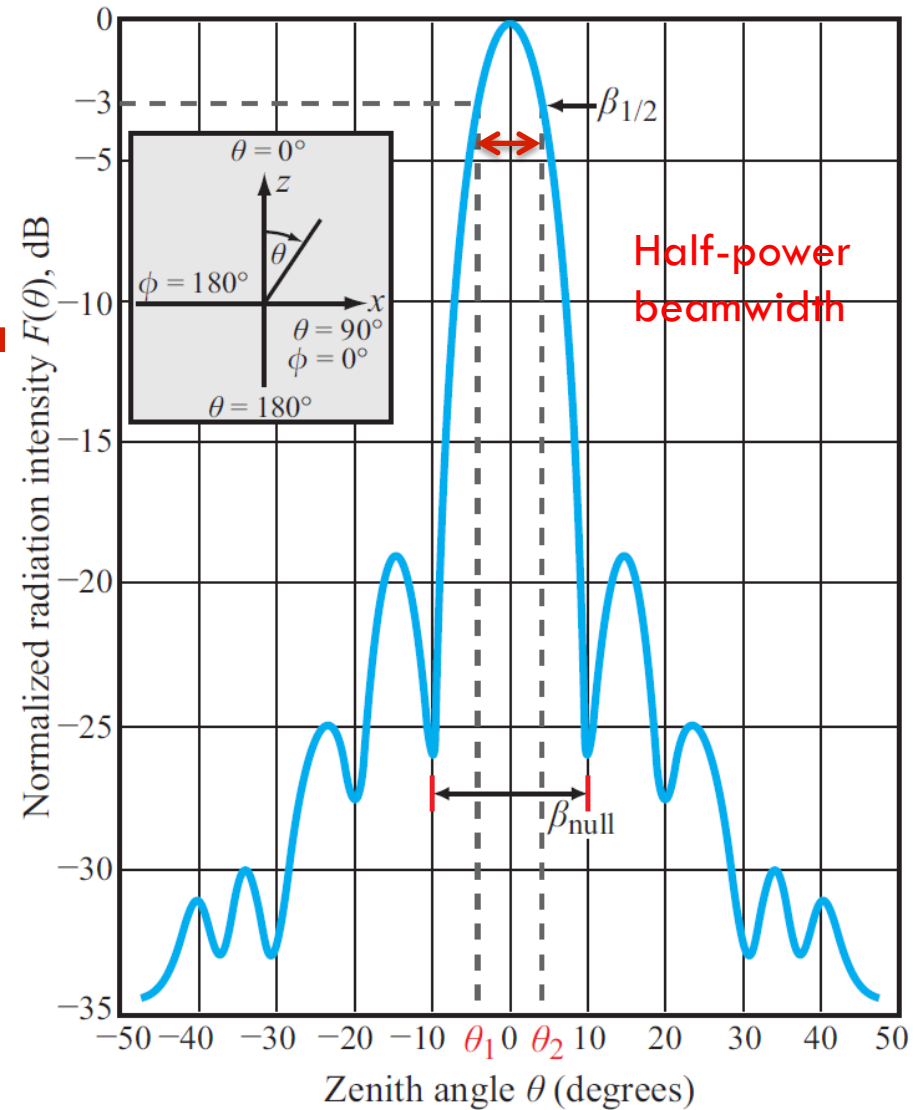
Radiation Pattern Beamwidth Dimensions

Null Bandwidth & Half-power beamwidth

$$\beta = \theta_2 - \theta_1,$$

where θ_1 and θ_2 are the *half-power angles* at which $F(\theta, 0) = 0.5$ (with θ_2 denoting the larger value and θ_1 denoting the smaller one,

Since 0.5 corresponds to -3 dB, the half power beamwidth is also called the 3-dB beamwidth.



Half-power angles:
theta1 and theta2

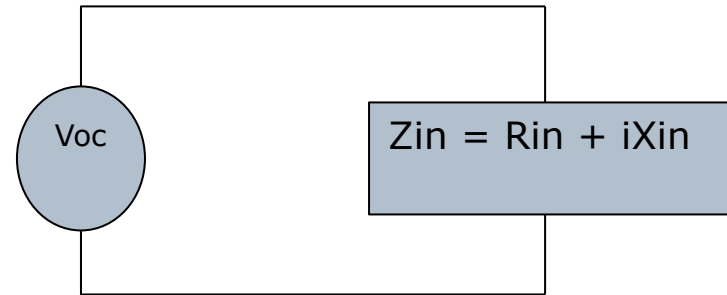
Antenna Radiation/Reception and Loss Resistances ($Z_{in} = R + jX$)

In this case: $R_{in} = R_{rad} + R_{loss}$
 Radiation resistance and loss resistance

We also have $P_t = P_{rad} + P_{loss}$

$$P_{rad} = \frac{1}{2} I_0^2 R_{rad},$$

$$P_{loss} = \frac{1}{2} I_0^2 R_{loss},$$



Circuit model for TX Antenna

$$\eta_{eff_receiver} = \frac{P_r}{P_{total}} = \frac{P_r}{P_r + P_{loss}} \quad \leftarrow \text{From the receiver point of view } P_r \text{ is power received)}$$

$$\eta_{eff_transmitter} = \frac{P_{rad}}{P_{total}} = \frac{P_{rad}}{P_{rad} + P_{loss}} = \frac{R_{rad}}{R_{rad} + R_{loss}}$$

Note:
 We want R_{loss} to be minimized!
 Also, when efficiency is 1 \rightarrow there is no loss!

Note that R_{rad} determines **the impedance matching** between the TX antenna and the source OR the RX antenna and the LOAD

Gain, Directivity, Power Radiated & Rrad

For any antenna:

$$P_{rad} = \frac{1}{2} I_0^2 R_{rad}$$

Directionality & Gain

$$D = \frac{4\pi R^2 S_{max}}{P_{rad}} = \frac{S_{max}}{S_{av}}$$

$$G = \eta_{eff} \cdot D$$

$$P_{rad} = \frac{4\pi R^2 S_{max}}{D}$$

Antenna Gain and Effective Area

Antenna	Power Gain	Effective Area
Isotropic	1	$\lambda^2/(4\pi)$
Small Dipole or Loop	1.5	$(1.5\lambda^2)/(4\pi)$
Half-Wave Dipole	1.64	$(1.64\lambda^2)/(4\pi)$
Horn, mouth area A	$(10A)/\lambda^2$	$0.81A$
Parabola, face area A	$(7A)/\lambda^2$	$0.56A$
Turnstile	1.15	$(1.15\lambda^2)/(4\pi)$

Assuming there is no ohmic loss (lossless antenna)

For the Hertzian dipole:

$$P_{rad} = \frac{4\pi R^2}{1.5} \times \frac{S_{max}}{R^2} \left(\frac{l}{\lambda}\right)^2 = 40\pi^2 I_0^2 \left(\frac{l}{\lambda}\right)^2$$

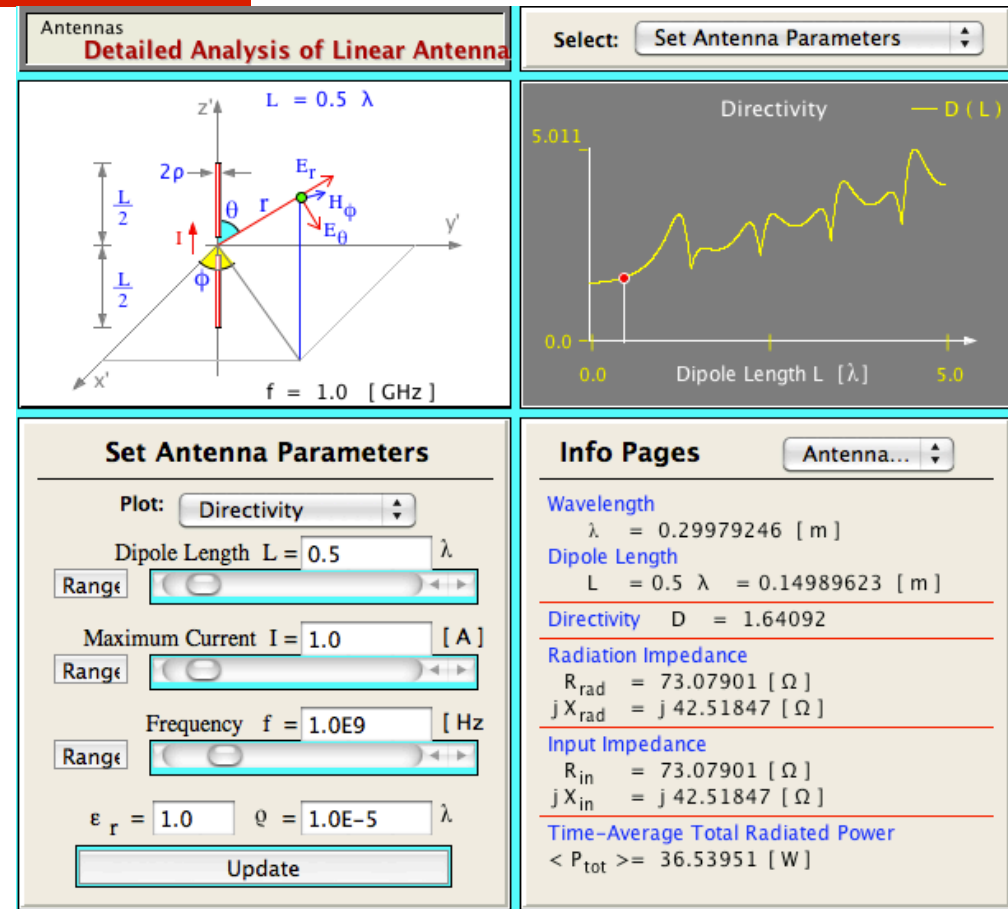
S_{max} is the average power radiated or pwr density radiated by an antenna

Power Gain = 1.5

$$R_{rad} = 80\pi^2 (l/\lambda)^2 \quad (\Omega).$$

Analyze a Dipole Antenna

- Set the current to 1 A
- Set length of the dipole to half wave
- What is the Rrad?
- What is Rin resistance?
- What is Directionality?
- What is the total radiate power?
- Go to "Scan Fields and Power",
 - Set ϕ equal to 90
 - Determine at which angle of θ we get max power
 - Determine at which angle of θ we get half power
 - What is the 3dB BW for this dipole?
- Answer the above questions but this time set the length to $\frac{1}{4}$ of the wave length.



Example

- Example C (Measuring the received power)
 - Example D (Resistance loss in a short dipole)
 - Example E (rewrite the average power density in terms of current, distance between the two antennas, length of the antenna, and frequency of operation for a short dipole (loop))
-

Review: Isotropic Antenna

- Radiated Power Approximation:

$$P_{rad} = EIPR = P_t \cdot G = \frac{4\pi d^2}{D} S_{max}$$

- Power Density (W/m²) is

$$S_{max} = E^2 / \eta_o = \frac{V^2 / m^2}{\Omega} = W / m^2$$

- For isotropic antennas $P_t = P_{rad}$

$$E = \frac{\sqrt{30P_t}}{d}$$

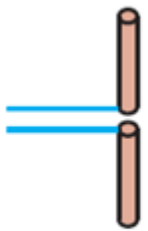
- Note that the free space impedance is ratio of E and H fields

$$H = \frac{\sqrt{P_t}}{68.8d}$$

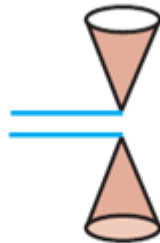
$$S_{max} = P_{den} = E \cdot H = \frac{P_t}{4\pi d^2}$$

$$\eta = E / H$$

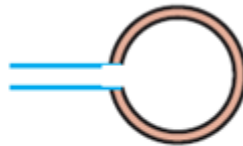
Different Antenna Types



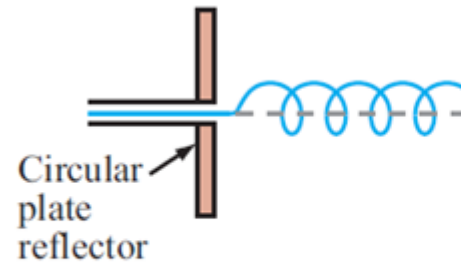
(a) Thin dipole



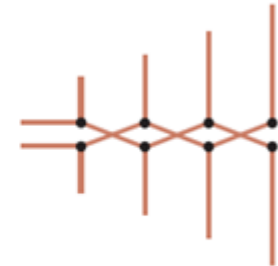
(b) Biconical dipole



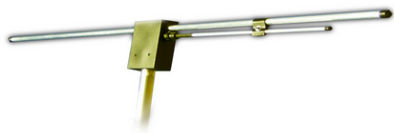
(c) Loop



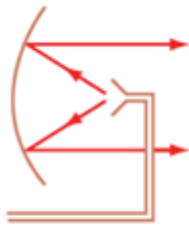
(d) Helix



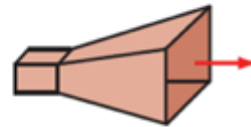
(e) Log-periodic



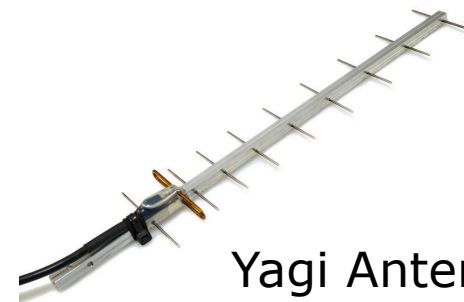
Dipole Antenna



(f) Parabolic dish reflector



(g) Horn



Yagi Antenna

Fields in Half-Wave Dipole

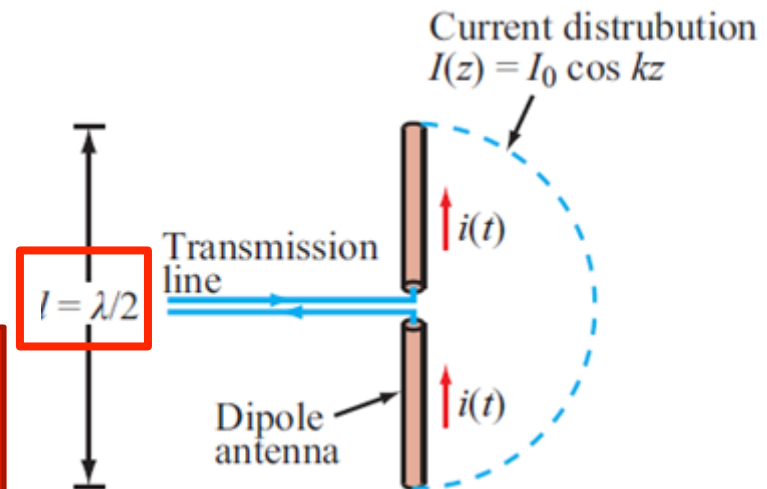
Homework Assignment

$$\tilde{E}_\theta = j 60 I_0 \left\{ \frac{\cos[(\pi/2) \cos \theta]}{\sin \theta} \right\} \left(\frac{e^{-jkR}}{R} \right),$$

$$\tilde{H}_\phi = \frac{\tilde{E}_\theta}{\eta_0} .$$

- **Example F:** Find the following:
- Find the expression for average power density
- Power Density (S_{max})
- Normalized radiation intensity, F
- Directionality, D (from the table)
- P_{radiated}
- R_{radiated}
- Prove that 3dB BW is in fact 78 degrees (you can use substitution to prove!)
- HINT: Use the applet to check your answers

All works must be shown!



Example: Complete the Table Below

Example G

Antenna	Gt=D	Rrad	Prad	3dB BW	Eff. Area
Isotropic	-----	-----	-----	-----	-----
Short Dipole					
1/2 Wave					
1/4 Wave	Later	Later	Later	Later	Later

Why $\text{dBi} = \text{dBd} + 2.15\text{dB}$? Explain!

References

- Ulaby, Fawwaz Tayssir, Eric Michielssen, and Umberto Ravaioli. *Fundamentals of Applied Electromagnetics: XE-AU....* Prentice Hall, 2001, Chapter 9
 - Black, Bruce A., et al. *Introduction to wireless systems.* Prentice Hall PTR, 2008, Chapter 2
 - Rappaport, Theodore S. *Wireless communications: principles and practice.* Vol. 2. New Jersey: Prentice Hall PTR, 1996, Chapter 3
 - Wheeler, Tom. *Electronic communications for technicians.* Prentice Hall, 2001. Section 12-1 & 12-2
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